# Effects of Various Parameters in Differential Scanning Calorimetry of Hydrogen-Peroxide-Treated Lignocellulose

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#### Synopsis

Differential scanning calorimetric (DSC) analyses of mixtures of hydrogen peroxide and lignocellulosic materials have been performed. The influence of chamber atmosphere composition, heating rate, pinhole size, lignocellulose particle size, and hydrogen peroxide-to-lignocellulose ratio were examined. With the exception of particle size, the variables produced significant effects on the DSC curves. These effects were mainly connected with changes in the atmosphere surrounding the sample, sample density, heat capacity, and heat conductance.

## **INTRODUCTION**

Differential scanning calorimetric analysis (DSC) of hydrogen peroxide and hydrogen-peroxide-treated lignocellulose was described in our previous two reports.<sup>1,2</sup> The samples were run at an elevated pressure in deactivated, hermetically sealed aluminum pans with a top pinhole. As with any transition process resulting from thermal treatment, numerous operational factors affect the nature and accuracy of thermal analysis. This report considers the impact of the major factors affecting determination of the thermal characteristics of  $H_2O_2$  decomposition and reactions between  $H_2O_2$  and lignocellulosic materials, including the composition of the chamber atmosphere, heating rate, pinhole size, particle size of lignocellulose, and hydrogen peroxide-to-wood ratio.

## **EXPERIMENTAL**

Unless otherwise stated, all materials used, methods of sample preparation, thermal analytical instrumentation, and operational procedures were the same as described in our previous report.<sup>2</sup> The DSC analyses were run using plain aluminum pans, deactivated by soaking in boiling 15% HNO<sub>3</sub> for 0.5 h followed by soaking in boiling 50%  $H_2O_2$  for 1 h, and finally washed several times with boiling water. The hermetically sealed pans were provided with a top pinhole between 0.050 and 0.065 mm in diameter. Prior to analysis the sample cell was purged with an appropriate gas at a flow rate of 50 mL/min at atmospheric or higher chamber pressures. The DSC runs were carried out at 975 psi pressure and 20°/min heating rate in nitrogen or oxygen atmospheres.

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## **RESULTS AND DISCUSSION**

#### Atmosphere of the Sample Chamber

It is well known that the rate and mechanism of reactions studied by DSC and involving lignocellulosic materials depend strongly on the composition of atmosphere immediately surrounding the sample and also within the chamber containing the sample holder. Atmospheric gases may react with the sample or displace volatile products of the reaction(s), changing the course and/or extent of reactions between such volatile products and the nonvolatile sample components. It is desirable, therefore, to control the composition of both the bulk gas and the gas immediately surrounding the sample. Unfortunately, due to the volatility of  $H_2O_2$  solution, it is impossible to remove the air entrapped in the sealed sample holder without changing the  $H_2O_2$  concentration in the sample. Therefore, only the composition of the bulk gas was controlled in this study.

Figures 1 and 2 and Table I show DSC results for  $H_2O_2$ -treated wood, lignin, cellulose, and pinitol (5-O—methyl *d*-inositol) run in  $N_2$  or  $O_2$ . The figures for specific areas (area/ $H_2O_2$  wt) represent averages of two measurements. As described in our previous report, the first exotherm is apparently due to two reactions,  $H_2O_2$  decomposition to form oxygen and water and reaction between  $H_2O_2$  and lignocellulose. As evidenced by Table I, the onset temperature  $T_0$  and the peak temperature  $T_1$  were unaffected by changing from pressurized  $N_2$  to pressurized  $O_2$ . However, such a change considerably reduced the  $T_1$  peak area and height. In the case of the  $T_2$  peak, shifting from  $N_2$  to  $O_2$  atmosphere increased the  $T_2$  peak temperature for  $H_2O_2$ -treated wood from 234.5°C to 253°C, while reducing the same for  $H_2O_2$ -treated cellulose from 251°C to 235°C. This indicates that cellulose is more susceptible to oxidation than lignin–carbohydrate complexes. Even more striking were the large increases in  $T_2$  peak areas in the case of  $H_2O_2$ -treated wood and cellulose and the appearance of a second exotherm

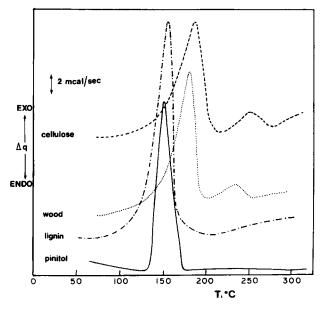


Fig. 1. DSC of H<sub>2</sub>O<sub>2</sub>-treated lignocellulose in N<sub>2</sub>; sample size, 1.42 mg.

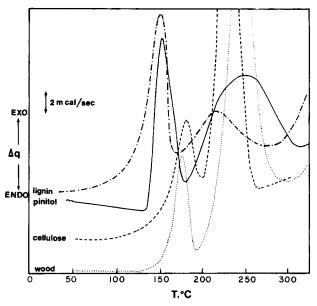


Fig. 2. DSC of  $H_2O_2$ -treated lignocellulose in  $O_2$ ; sample size, 1.42–3.55 mg.

 $(T_2)$  in the cases of H<sub>2</sub>O<sub>2</sub>-treated lignin and pinitol now partially overlapping the first exotherm.

With  $H_2O_2$ -treated cellulose and wood, the enhancement of  $T_2$  peak areas in  $O_2$  indicates that the second exothermal reaction involves oxygen. This is supported by the appearance of the second exotherm in DSC of  $H_2O_2$ -treated lignin and pinitol run in  $O_2$  atmosphere. The much larger  $T_2$  peak areas associated with  $H_2O_2$ -treated wood and cellulose as compared to  $H_2O_2$ -treated lignin in  $O_2$  suggest that carbohydrates are primarily responsible for the second exothermal reaction in  $N_2$ .

Table I also includes data on the thermal characteristics of  $H_2O_2$  decomposition in  $N_2$  and  $O_2$  atmosphere. The results indicate that, although the maximum decomposition temperature of  $H_2O_2$  (50% w/w) was unaffected by shifting from  $N_2$  to  $O_2$  atmosphere, such a change decreased the onset temperature ( $T_0$ ).

## **Heating Rate**

Heating rate can assume a major importance when studying chemical reactions by thermal analysis.<sup>3,4</sup> The results shown in Figures 3, 4, and 5 indicate that increasing the heating rate from 10°C/min to 50°C/min does not significantly affect the characteristics of the first or second exotherm obtained by DSC of  $H_2O_2$ ,  $H_2O_2$ -treated lignin, or  $H_2O_2$ -treated carbohydrates in N<sub>2</sub>. However, DSC of carbohydrates run at slower heating rates of 2–5°C/min, while showing the first exothermic peak similar to that obtained at higher heating rates, does not show the second exothermic peak.

The absence of the second exothermic peak at slower heating rates in  $N_2$  is consistent with the work of Johnson and Miller,<sup>5</sup> who suggested that faster heating rates may sometimes be required to observe minor reactions not detectable at slower heating rates. Interestingly, the second exothermic peak is

-			First peak		Secon	d peak
	Materials	Onset temp. T <sub>0</sub> (°C)	Peak temp. T <sub>1</sub> (°C)	Specific area (cm <sup>2</sup> /mg H <sub>2</sub> O <sub>2</sub> )	Peak temp. T <sub>2</sub> (°C)	Specific area (cm <sup>2</sup> /mg carbohy.)
	H <sub>2</sub> O <sub>2</sub> -treated					
in nitrogen	Lignin (brown rot)	125	154	48.91	_	
	Wood (extractive free, white fir)	147.5	182	37.94	232	2.81 <sup>b</sup>
	Cellulose (microcrys- talline)	151	186	35.97	250	2.12
	Arabinoxylan	122.5	140	37.76	202	6.91
	Pinitol	135	152	32.66	_	
	Glucose	103	135	36.35	244	3.71
	H <sub>2</sub> O <sub>2</sub> (50 wt %)	137	187	14.11		
	Wood exo. shoulder at exo. shoulder at		ndo. peak at S	385°C, exo. pe	ak at 405°C,	
in oxygen	H <sub>2</sub> O <sub>2</sub> -treated					
	Lignin	126	153	39.51	220	8.76 <sup>c</sup>
	Wood	157	182	29.11	253	33.65 <sup>b</sup>
	Cellulose	153	185	28.33	235	46.90
	Pinitol	135	152	31.90	234	8.10
	Glucose	118	140	29.63	238	27.25
	H <sub>2</sub> O <sub>2</sub> (50 wt %)	126	183	13.47		
	Wood	exo. peak	s at 339°C ar	nd 477°C		

TABLE I Thermal Behavior of  $H_2O_2$  and  $H_2O_2$ -Treated Lignocellulosic Materials in  $N_2$  and  $O_2^a$ 

<sup>a</sup> Heating rate: 20°C/min, pressure: 975 psi, pinhole plain aluminum pan.

<sup>b</sup> Assuming 75% of white fir is carbohydrate.

<sup>c</sup> Based on lignin.

observed with  $H_2O_2$ -treated materials at all heating rates examined, when DSC is performed in  $O_2$  (Figs. 6 and 7). The absence of the second exothermic peak at lower heating rates in  $N_2$  suggests that the second exothermic reaction is not only a function of carbohydrate content, but also of  $O_2$  supply. The oxygen may result from the thermal decomposition of hydrogen peroxide  $(2H_2O_2 \rightarrow 2H_2O$  $+ O_2)$  or could also be a product of some reaction between hydrogen peroxide and lignocellulose. Apparently at slower heating rates, the rate of  $O_2$  production is too slow, compared to the rate of  $O_2$  exchange with the surrounding  $N_2$  atmosphere, to permit a significant oxygen-carbohydrate reaction. Such a reaction is observed at higher heating rates, where  $O_2$  is produced faster and becomes available for the reaction prior to exchange.

## **Pinhole Size**

The structure of the sample holder is extremely important to DSC of materials such as  $H_2O_2$ -treated wood where volatile products are formed during analysis. In this case, the shape and thermal characteristics of DSC curves are determined by the temperature dependent rate of  $H_2O_2$  evaporation. The DSC results depend also on the size of the opening in the top of the sample holder through which reactive vapors escape during analysis. The size of the opening regulates also

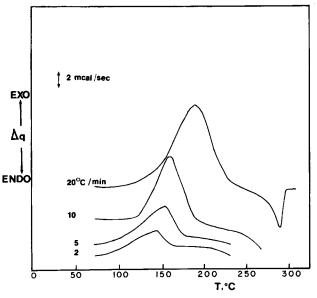


Fig. 3. DSC of 50 wt %  $H_2O_2$  at different heating rates in  $N_2$ ; sample size, 1.89 mg.

the extent to which volatile products are displaced by purging gas. Specifically in the case of  $H_2O_2$ -treated wood, the size of the pinhole can influence the reaction of carbohydrate components of wood with  $O_2$  produced from  $H_2O_2$  and represented by the second exothermic peak observed between 220–250°C at 975 psi, in  $N_2$  atmosphere.

The effect of the size of the pinhole on the DSC characteristics of  $H_2O_2$ -treated wood in  $N_2$  at atmospheric pressure is shown in Figure 8. Increasing the pinhole size from 0.050 to 0.255 mm resulted in broadening of the evaporation endotherm and a lower evaporation initiation temperature for the aqueous  $H_2O_2$  component

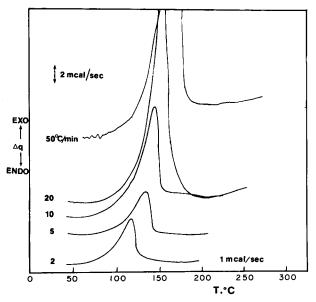


Fig. 4. DSC of H<sub>2</sub>O<sub>2</sub>-treated lignin at different heating rates in N<sub>2</sub>; sample size, 1.89 mg.

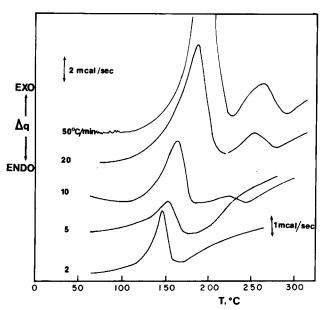


Fig. 5. DSC of H<sub>2</sub>O<sub>2</sub>-treated cellulose at different heating rates in N<sub>2</sub>; sample size, 1.89 mg.

of the system. The evaporation initiation temperature was lowered even more when the sample pan was opened. Increasing the pinhole size also had a striking effect on the characteristics of the first exothermal peak, which occurred at 160°C under atmospheric pressure. As mentioned previously, this exotherm results

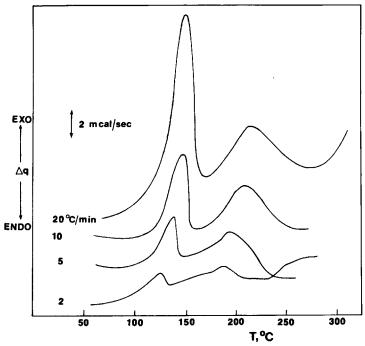


Fig. 6. DSC of lignin at different heating rates in  $O_2$ ; sample size, 1.89 mg.

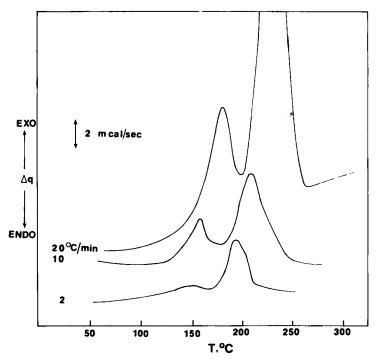


Fig. 7. DSC of cellulose at different heating rates in O<sub>2</sub>; sample size, 1.89 mg.

from two reactions, decomposition of  $H_2O_2$  vapor and reaction of  $H_2O_2$  vapor with wood. As the pinhole size was increased, the size of this exothermal peak (area per unit weight of  $H_2O_2$ ) decreased to the point of its disappearance in the case of the open pan. These findings indicate that larger pinhole openings allow

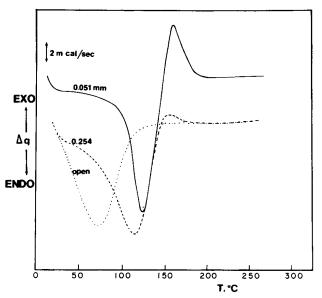


Fig. 8. DSC of  $H_2O_2$ -treated wood at different pinhole sizes, in  $N_2$ , at ambient pressure; sample size, 1.89 mg.

greater amounts of  $H_2O_2$  vapor to escape from the sample holder yielding less  $H_2O_2$  vapor available for decomposition or reaction with wood.

At 975 psi, and in either  $N_2$  or  $O_2$ , the effect of pinhole size on the first exothermal peak of  $H_2O_2$ -treated wood differed from that observed for  $N_2$  at ambient pressure. Figures 9 and 10 show that the shape and area of the first exotherm when measured at 975 psi did not significantly change when the pinhole size was varied from 0.050 to 1.125 mm in  $N_2$  atmosphere or from 0.050 to 1.143 mm in  $O_2$  atmosphere. However, larger openings affected the shape and area of this peak. Thus, with an opening of 1.990 mm the first exothermal peak in either  $N_2$  or  $O_2$  atmosphere became broader and less sharp. Moreover, when the pan was completely open, the sharp exotherm observed with pinholes below 1.125 mm became an extended exothermal shoulder.

The size of the pinhole did not significantly affect the shape or area of the second exothermal peak of  $H_2O_2$ -treated wood when run in  $O_2$  at 975 psi; however, it did so in  $N_2$  (Fig. 9). In this case, as pinhole size was increased from 0.060 to 0.635 mm, the peak areas decreased. For a 0.635-mm pinhole, the second exothermal peak occurred only as a shoulder, and, with the pan completely open, no second peak was observed at all. Since the second exothermal peak results from the reaction of wood components with  $O_2$ , either trapped in the sample pan or produced during the first exothermal reaction(s), these results indicate that the available oxygen is gradually displaced from the pan atmosphere by the surrounding  $N_2$ , the displacement taking place more rapidly at larger pinhole openings.

The results are consistent with the findings of Miller and Turner,<sup>6</sup> who analyzed by DTA the thermal behavior of cellulose at ambient pressure in  $N_2$  atmosphere. When the sample was encapsulated in air using a sealed sample pan provided with a top pinhole, they observed a small exothermal peak at 325°C; this peak was absent, however, when the sample pan was completely open or when

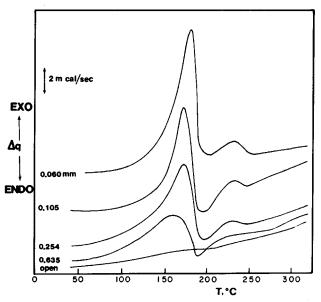


Fig. 9. DSC of  $H_2O_2$ -treated wood at different pinhole sizes, in  $N_2$ , at 975 psi pressure; sample size, 1.89 mg.

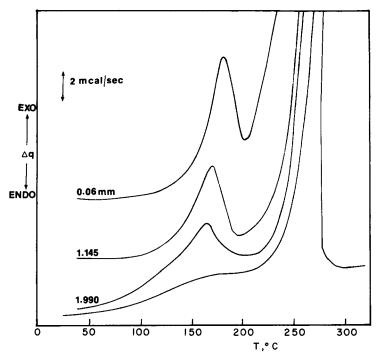


Fig. 10. DSC of  $H_2O_2$ -treated wood at different pinhole sizes, in  $O_2$ , at 975 psi pressure; sample size, 1.89 mg.

the sample was encapsulated in N<sub>2</sub>. The difference between the chamber pressure used in the present study (975 psi) and that used in the study of Miller and Turner (14.7 psi) explains the difference between the exothermal peak temperatures observed. The difference in the magnitude of the exotherm observed at 325°C by Miller and Turner and the magnitude of the exotherm observed at 220–250°C in the present study can be also explained by taking into account the relative amounts and concentrations of O<sub>2</sub> available for reaction with carbohydrate macromolecules. In the Miller and Turner work, trapped O<sub>2</sub> was the only source of O<sub>2</sub>, while, in the present work, O<sub>2</sub> resulted also from the H<sub>2</sub>O<sub>2</sub> reactions.

A discussion of the influence of the condition of the top of the sample holder

	First peak			Second peak		
Particle mesh size	Onset temp (°C)	Peak temp (°C)	Specific peak area (cm <sup>2</sup> /mg H <sub>2</sub> O <sub>2</sub> )	Peak temp (°C)	Specific peak area (cm <sup>2</sup> /mg OD wood)	
<200	145.5	171.0	34.415	221.0	1.324	
80-100	154.0	173.0	34.415	227.5	1.580	
60-80	147.5	175.5	37.532	229.0	1.616	
40-60	145.5	175.0	39.979	231.5	2.209	
20-40	144.0	178.0	39.431	229.0	1.616	

TABLE II Effect of Particle Size on DSC Characteristics of Hydrogen-Peroxide-Treated Wood<sup>a</sup>

<sup>a</sup> Heating rate: 20°C/min; pressure: 975 psi; pinhole plain aluminum pan; sample weight, 1.89 mg.

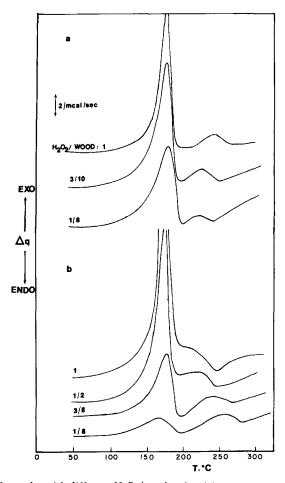


Fig. 11. DSC of samples with different  $H_2O_2$ /wood ratios, (a) constant amount of  $H_2O_2$  and (b) constant total sample weight;  $N_2$  atmosphere; sample size, 1.05–3.55 mg.

on DSC of the decomposition of various fibers in air and in N<sub>2</sub> at ambient pressure is included in the work by Ennis.<sup>7</sup>

### **Particle Size**

Particle size of samples is an important parameter in thermal analysis, particularly in characterization of chemical reactions. As a general rule, chemical reactivity increases as particle size decreases. In DSC, this is evidenced by a sharpening of the peaks as the particle size is decreased. DSC peak area is also inversely proportional to thermal conductivity of the sample which depends in turn on both particle size and packing density.<sup>8</sup>

Table II presents results showing the effect of particle size on DSC characteristics of  $H_2O_2$ -treated wood. The experiments were made by thoroughly mixing five parts vacuum/oven-dried samples of deionized wood of different particle sizes (i.e., <200 to 20–40 mesh) with three parts 50% w/w  $H_2O_2$  in the manner described in our previous paper.<sup>1</sup> The treated samples were stored at

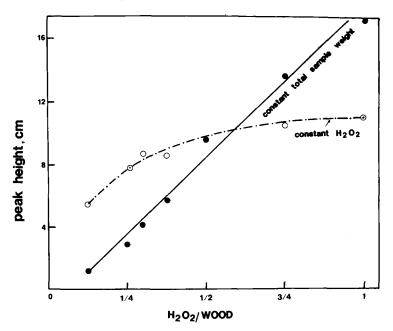


Fig. 12. Relationship between peak height and H<sub>2</sub>O<sub>2</sub>/wood ratio. First exothermal peak.

ambient temperature for 16 h in closed weighing containers prior to the runs. The results showed no major differences between the thermal behavior of  $H_2O_2$ -treated wood in the range of particle sizes of <200 to 20–40 mesh, although there was a discernible slight drop in the maximum peak temperatures and peak areas with a decrease in particle size for both exothermal ( $T_1$  and  $T_2$ ) reactions.

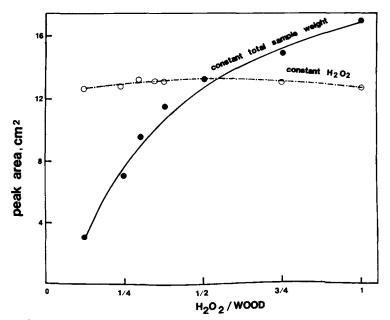


Fig. 13. Relationship between peak area and H<sub>2</sub>O<sub>2</sub>/wood ratio. First exothermal peak.

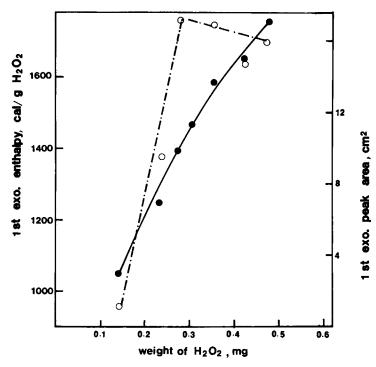


Fig. 14. Dependence of enthalpy and peak area on the amount of  $H_2O_2$  at a constant total sample weight = 1.42 mg. First exothermic peak. (- $\bullet$ -) Area; (-.  $\circ$ -.-) enthalpy.

#### H<sub>2</sub>O<sub>2</sub>-Lignocellulose Ratio

For investigation of the influence of concentration of the reactants, the deionized 60–80 mesh wood samples were extracted with boiling alcohol and water, mixed with 50% w/w  $H_2O_2$  at different  $H_2O_2$ /wood ratios and stored at ambient temperature in a closed weighing container for 8 h before thermal analysis. Mixtures of  $H_2O_2$  and wood were prepared either by adding a constant amount of  $H_2O_2$  (equivalent to 0.35 mg of anhydrous  $H_2O_2$ ) to different quantities of wood (method 1), or by adding different quantities of  $H_2O_2$  to wood to produce a constant total sample weight (method 2). The effect of the  $H_2O_2$ /wood ratio on the thermal characteristics of  $H_2O_2$ -treated wood is shown in Figures 11–15 (N<sub>2</sub> atmosphere).

With samples prepared by method 1, varying the  $H_2O_2/wood$  ratio between 1/8 and 1 resulted in little or no effect on the first exothermal peak area, temperature or enthalpy (Fig. 13). At the same time, increase in the  $H_2O_2/wood$  ratio resulted in an enhanced reactivity, as evidenced by peak sharpening with the peak height increasing with an increasing  $H_2O_2/wood$  ratio up to a ratio of 1/2, and then remaining relatively constant (Figs. 11 and 12). Varying the  $H_2O_2/wood$  ratio between 1/8 to 1 slightly increased the maximum temperature of the second exothermal peak without affecting its shape or area (Fig. 15). The lower peak temperatures of the second exotherm observed at lower  $H_2O_2/wood$  ratios can be accounted for by the relatively greater proportion of carbohydrates.

When  $H_2O_2$ -wood mixtures of different constituent ratios were prepared to yield a constant total sample weight (method 2), considerable variation in the

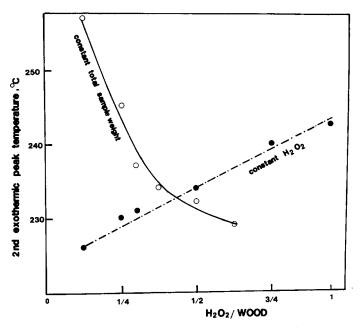


Fig. 15. Relationship between maximal peak temperature and H<sub>2</sub>O<sub>2</sub>/wood ratio. Second exothermic peak.

thermal behavior of the mixtures was observed. Both the first and second exothermal peaks were broader with the second exothermal peak overlapped by an endotherm [Fig. 11(b)]. In the case of the first exotherm, the peak height was a linear function, and the peak area an exponential function of the H<sub>2</sub>O<sub>2</sub>/wood ratio (Figs. 12 and 13). The temperature of the first exothermal peak increased with increasing H<sub>2</sub>O<sub>2</sub>/wood ratio between 1/8 and 3/8, and then remained relatively constant up to a ratio of 1. This is consistent with the work of Melling et al.<sup>8</sup> and Barrall and Rogers,<sup>3</sup> who showed that peak temperature is not a function of thermal conductivity, but rather increases slightly with increasing density and specific heat. Increasing the H<sub>2</sub>O<sub>2</sub>/wood ratio while keeping the total mixture weight constant increases the density and heat capacity of the mixture because the density and heat capacity of H<sub>2</sub>O<sub>2</sub> (50% w/w) is about three to four times larger than that of oven-dried wood (H<sub>2</sub>O<sub>2</sub> 50% w/w: density = 1.1914 g/cc at 25°C; heat capacity = 0.790 cal/g-soln-°C at 27°C<sup>9</sup>; oven-dried white fir: density = 0.38 g/cc; heat capacity = 0.257 cal/g-°C at 27°C).<sup>10</sup>

With mixtures prepared by method 2, the second exotherm, unlike the first exotherm, showed a decrease in peak temperature with an increasing  $H_2O_2/wood$  ratio, apparently due to the presence of higher  $O_2$  concentrations at higher ratios. The second exotherm was broader at low  $H_2O_2$  wood ratios and was overlapped by an endotherm at high ratios. This endotherm corresponds to water evaporation (water from 50% w/w  $H_2O_2$  solution and from  $H_2O_2$  decomposition).

The thermal properties of an exothermic process are determined not only by the thermal properties of the sample, but also by the thermal conductivity between the sample and sample holder and the sample holder and platform. Unlike endothermic processes, which always set up transition fronts, an exothermic reaction liberates heat which can cause the sample temperature to rise above that of the heating platform creating a gradient whereby heat can transfer from the sample to the platform. With mixtures prepared by method 1, the same amount of  $H_2O_2$  was distributed over a larger amount of wood as the  $H_2O_2/wood$  ratio was decreased. Thus, at lower  $H_2O_2/wood$  ratios, the heat transfer path was much less continuous and the amount of  $H_2O_2$  (liquid) available at the surface was greatly reduced as compared with the higher  $H_2O_2/wood$  ratios. At  $H_2O_2/wood$  ratios below 1/2 this was evidenced by smaller peak heights, indicative of reduced reactivity. When the mixtures were prepared by method 2, the increased quantity of  $H_2O_2$  at a constant total sample weight resulted in more continuous heat transfer and greater surface contact between the sample and the sample holder at higher  $H_2O_2/wood$  ratios. This was evidenced by a linear increase in peak height with an increasing  $H_2O_2/wood$  ratio.

It is important to note that the total heat of reaction was relatively constant for samples prepared by method 1, in which the same quantity of  $H_2O_2$  was added per sample mixture, while the total heat of reaction increased for an  $H_2O_2$ /wood ratio of 1/8 to 3/8 and then remained relatively constant for an  $H_2O_2$ /wood ratio up to 1, when the mixtures were prepared by adding increasing quantities of  $H_2O_2$ per total sample weight (Figs. 13–14). In the latter case, the reduced enthalpy values at lower  $H_2O_2$ /wood ratios were partially the result of reduced heat capacity at lower  $H_2O_2$ /wood ratios.

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